



Norwegian University of
Science and Technology

Model-Based Identification of Nanomechanical Properties in Atomic Force Microscopy

Michael R. P. Ragazzon, Jan Tommy Gravdahl, Kristin Y. Pettersen

Department of Engineering Cybernetics,
NTNU, Norwegian University of Science and Technology

MARSS 2019, Helsinki, Finland,
July 1–5, 2019

Outline

Introduction

System modeling

Parameter identification

Experiments

Conclusion

Outline

Introduction

System modeling

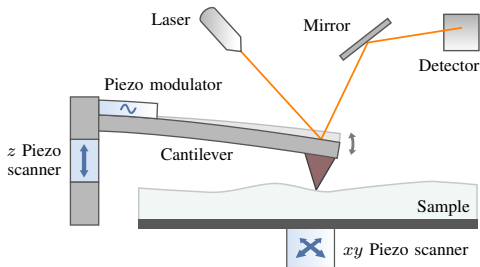
Parameter identification

Experiments

Conclusion

Introduction

- Atomic force microscopy (AFM) is capable of measuring forces into the piconewton range.



Introduction

- Traditionally, static cantilever deflection used to resolve elastic properties.
- More recently, single- and multifrequency approaches allow dynamic (elastic and viscous) properties to be gathered.

Introduction

- Traditionally, static cantilever deflection used to resolve elastic properties.
 - More recently, single- and multifrequency approaches allow dynamic (elastic and viscous) properties to be gathered.
 - However, interaction forces are inherently nonlinear and often requires:
 - linearization
 - multifrequency demodulation
 - consideration of harmonics
- to relate the observables to mechanical properties.

Introduction

- Traditionally, static cantilever deflection used to resolve elastic properties.
 - More recently, single- and multifrequency approaches allow dynamic (elastic and viscous) properties to be gathered.
 - However, interaction forces are inherently nonlinear and often requires:
 - linearization
 - multifrequency demodulation
 - consideration of harmonics
- to relate the observables to mechanical properties.
- In our work, we propose a method to relate the nanomechanical properties directly from the observables using the time-domain dynamic models.

Overview of proposed method

- Find the dynamic model of the cantilever.
 - Well known, linear model.

Overview of proposed method

- Find the dynamic model of the cantilever.
 - Well known, linear model.
- Find a relationship between tip-sample interaction force and sample parameters.
 - Nonlinear, and material-dependent. Non-trivial.

Overview of proposed method

- Find the dynamic model of the cantilever.
 - Well known, linear model.
- Find a relationship between tip-sample interaction force and sample parameters.
 - Nonlinear, and material-dependent. Non-trivial.
- Combine the cantilever and sample model.

Overview of proposed method

- Find the dynamic model of the cantilever.
 - Well known, linear model.
- Find a relationship between tip-sample interaction force and sample parameters.
 - Nonlinear, and material-dependent. Non-trivial.
- Combine the cantilever and sample model.
- Use parameter identification techniques to relate the observables to sample parameters.

Outline

Introduction

System modeling

Parameter identification

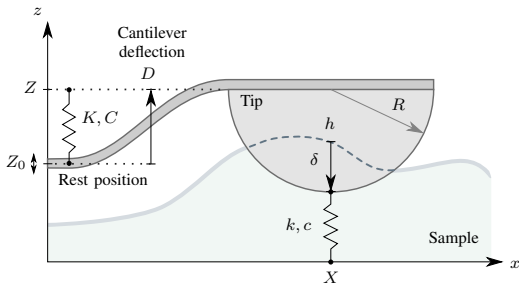
Experiments

Conclusion

Cantilever dynamics

Approximation by first resonance mode.

$$M\ddot{D} + KD + C\dot{D} = F_{\text{mod}} + F_{\text{ts}}. \quad (1)$$



Contact model

Modified Hertz contact model.

$$F_{ts} = E' \delta^{\frac{3}{2}} + c\dot{\delta} \quad (2)$$

$$E = \frac{3}{4} R^{-\frac{1}{2}} (1 - \nu^2) E' \quad (3)$$

Outline

Introduction

System modeling

Parameter identification

Experiments

Conclusion

Parametric model

Combining the previous cantilever and sample models gives the system

$$Ms^2D + CsD + KD - F_{\text{mod}} = cs\delta + E'\delta^{1.5}. \quad (4)$$

Parametric model

Combining the previous cantilever and sample models gives the system

$$Ms^2D + CsD + KD - F_{\text{mod}} = cs\delta + E'\delta^{1.5}. \quad (4)$$

Define

$$w' \triangleq Ms^2D + CsD + KD - F_{\text{mod}} \quad (5)$$

and rewrite (4) as

$$w' = \begin{bmatrix} c \\ E' \end{bmatrix}^T \begin{bmatrix} s\delta \\ \delta^{1.5} \end{bmatrix} \quad (6)$$

$$= \theta^T \phi' \quad (7)$$

which gives the parametric formulation of the sample model.

Parametric model

Combining the previous cantilever and sample models gives the system

$$Ms^2D + CsD + KD - F_{\text{mod}} = cs\delta + E'\delta^{1.5}. \quad (4)$$

Define

$$w' \triangleq Ms^2D + CsD + KD - F_{\text{mod}} \quad (5)$$

and rewrite (4) as

$$w' = \begin{bmatrix} c \\ E' \end{bmatrix}^T \begin{bmatrix} s\delta \\ \delta^{1.5} \end{bmatrix} \quad (6)$$

$$= \theta^T \phi' \quad (7)$$

which gives the parametric formulation of the sample model.

Persistently exciting $\phi \rightarrow$ exponential convergence of parameters.

Parameter estimator

Least squares method with forgetting factor (Ioannou and Sun 1996).

$$\hat{w} = \hat{\theta}^T \phi \quad (8)$$

$$\varepsilon = (w - \hat{w})/m^2 \quad (9)$$

$$m^2 = 1 + \alpha \phi^T \phi \quad (10)$$

$$\dot{\hat{\theta}} = \mathbf{P} \varepsilon \phi \quad (11)$$

$$\dot{\mathbf{P}} = \beta \mathbf{P} - \mathbf{P} \frac{\phi \phi^T}{m^2} \mathbf{P} \quad (12)$$

$$\mathbf{P}(0) = \mathbf{P}_0 \quad (13)$$

Outline

Introduction

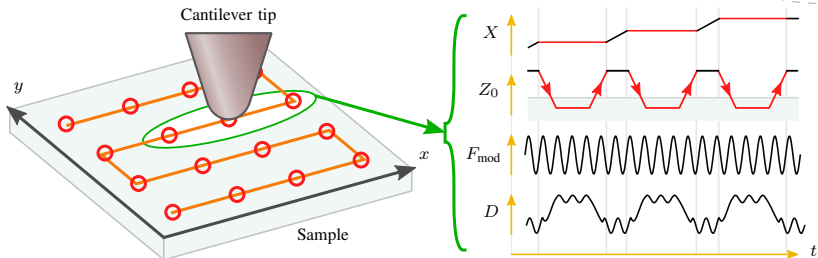
System modeling

Parameter identification

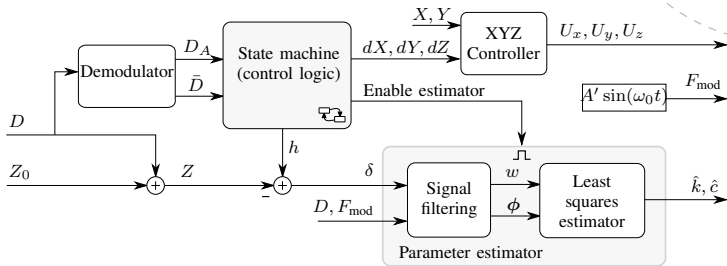
Experiments

Conclusion

Procedure



Experimental setup

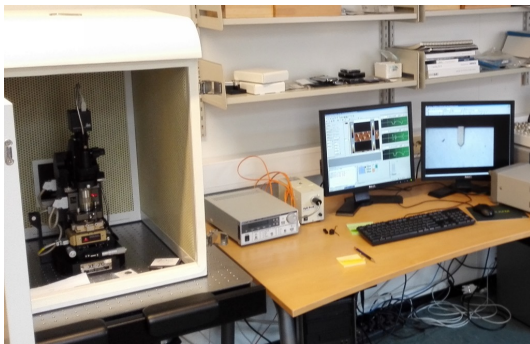


Block diagram of the control logic and parameter estimator.

Experimental setup

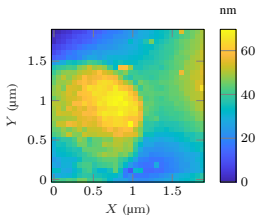
- Implemented on a commercial AFM, Park Systems XE-70.
- All aspects controlled by our own algorithms.
- Real-time implementation at 200 kHz on a dSpace computer.
- Spherical carbon tip cantilever, radius 40 nm (B40_CONTR).
- Cantiler parameters M , K , C determined a priori.

Experimental setup

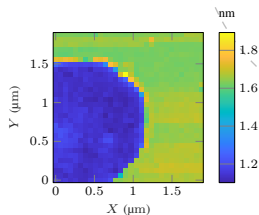


Park Systems XE-70 AFM and setup.

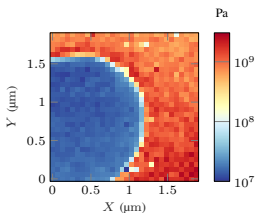
Experimental results: Two-component polymer sample



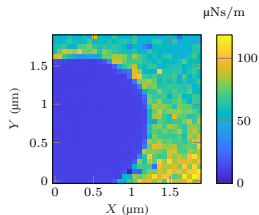
(a) Topography



(b) Amplitude

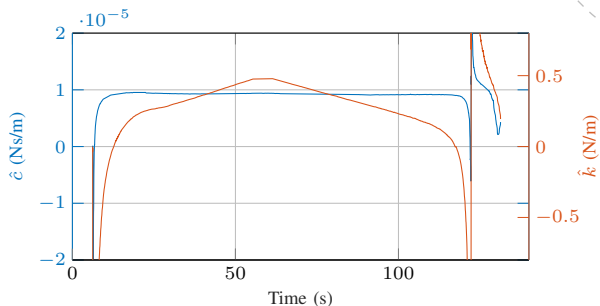


(c) Elastic modulus



(d) Damping coefficient

Experimental results: Time-varying parameters



Time-varying sample parameter estimates during indentation.

Outline

Introduction

System modeling

Parameter identification

Experiments

Conclusion

Conclusion

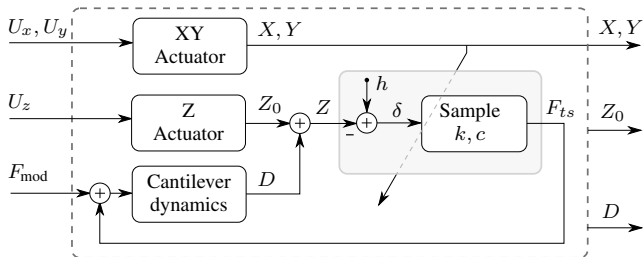
- Online, model-based identification technique for nanomechanical properties.
- Sample parameters are mapped from observables in a least squares sense.
- Handles nonlinear force interactions naturally.
- Time-domain approach, circumvents the need
 - for linearization,
 - to consider harmonics,
 - demodulation, either single- or multifrequency.
- Can modify the cantilever and sample dynamics separately.

Conclusion



- Online, model-based identification technique for nanomechanical properties.
- Sample parameters are mapped from observables in a least squares sense.
- Handles nonlinear force interactions naturally.
- Time-domain approach, circumvents the need
 - for linearization,
 - to consider harmonics,
 - demodulation, either single- or multifrequency.
- Can modify the cantilever and sample dynamics separately.

Questions?

Plant dynamics



Bibliography I

-  Ioannou, P A and J Sun (1996). "Robust Adaptive Control". Upper Saddle River, NJ: Prentice Hall.
-  Ragazzon, M.R.P., J.T. Gravdahl, and K.Y. Pettersen (2018). "Model-Based Identification of Nanomechanical Properties in Atomic Force Microscopy: Theory and Experiments". *IEEE Transactions on Control Systems Technology*.